SmartAnswer – Investigations of stream-wise Rod Vortex Generators effect on noise generated by boundary layer separation on blades. T. Suresh¹, P. Flaszynski², O. Szulc³ ¹PhD Candidate, ²Professor, ³Senior Researcher, Department of Aerodynamics ¹²³Institute of Fluid- Flow Machinery, Polish Academy of Sciences



Smart Mitigation of flow-induced Acoustic Radiation and Transmission for reduced Aircraft, surface traNSport, Workplaces and wind en ERgy noise





Host institution

Institute of **Fluid- Flow** Machinery, PAN

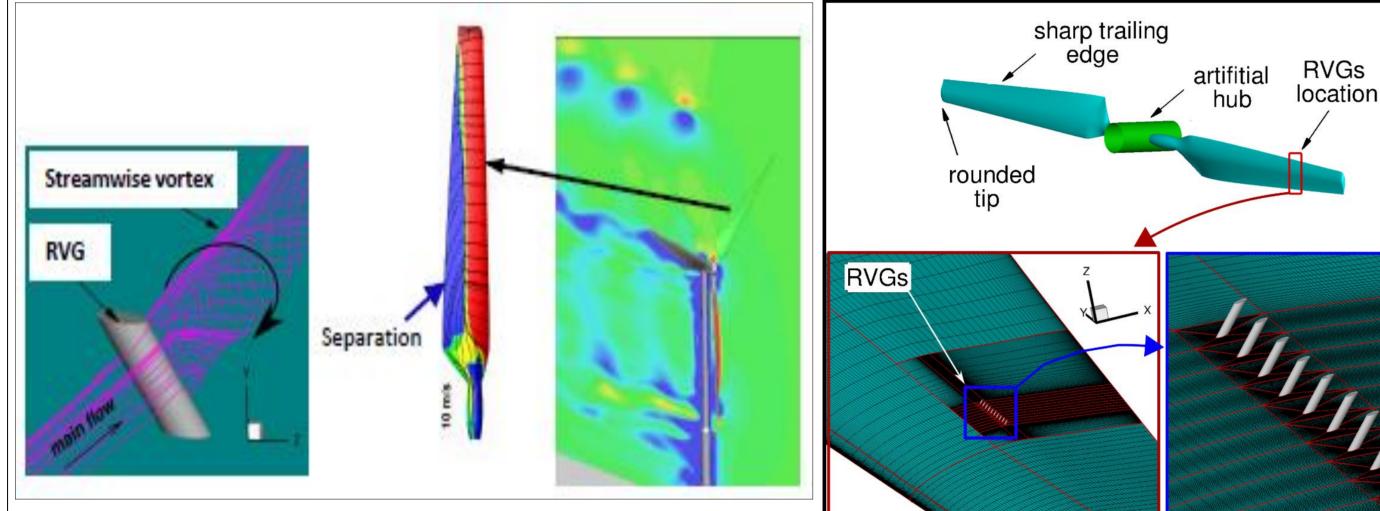


Partnership

Theory: Integral solution of FW-H by Farassat as Formulation 1A^[2] $4\pi p'_{T}(x,t) = \int_{f=0}^{I} \left[\frac{\rho_{0} \dot{v}_{n}}{r(1-M_{r})^{2}} + \frac{\rho_{0} v_{n} \hat{r}_{i} \dot{M}_{i}}{r(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_{n} (M_{r} - M^{2})}{r^{2}(1-M_{r})^{3}} \right]_{rot} dS + \int_{f=0}^{I} \left[\frac{\rho_{0} c v_$ Thickness near –field term Thickness far -field term $\left|4\pi p'_{L}(x,t) = \int_{f=0}^{\infty} \left[\frac{\dot{p}\cos\theta}{cr(1-M_{r})^{2}} + \frac{\hat{r}_{i}\dot{M}_{i}p\cos\theta}{cr(1-M_{r})^{3}}\right] dS + \frac{dS}{cr(1-M_{r})^{3}} dS + \frac{dS}{cr(1-M_{r})^{3}}\right]$ Loading near –field term $\int_{f=0} \left[\frac{p(\cos\theta - M_i n_i)}{r^2 (1 - M_r)^2} + \frac{(M_r - M^2) p \cos\theta}{r^2 (1 - M_r)^3} \right] dS$ Loading far –field term Analysis: Stationary : Monopole/Thickness Validation and **Dipole**/loading

Motivation

- One of the challenges for **wind energy** is to overcome the **noise** complaint of the residents living near wind farms.
- Trailing edge noise has been studied intensively for design cases.
- Flow separation occurs in higher wind speed cases leading to decreased performance of wind turbines in off-design conditions.



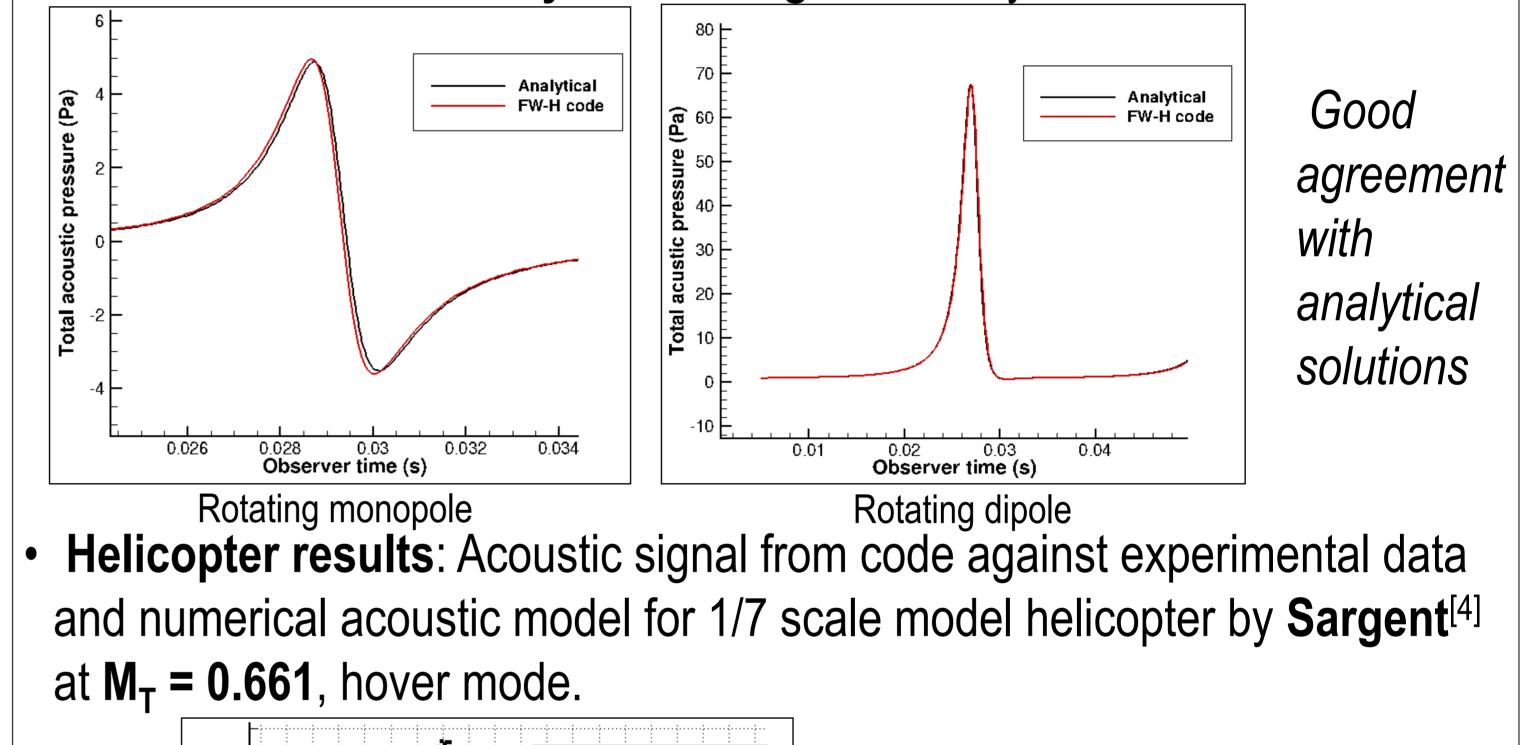
Flow visualization on wind turbine blade with RVGs^[1]

- Rod Vortex Generators(RVGs) are investigated to reduce the flow separation.
- **RVGs increase aerodynamic performance** of wind turbine and helicopter rotors.

- Rotating : Monopole, Dipole, source sink pair Helicopter rotor case – experimental and other numerical results available(thickness term dominant).
- Wind turbine blade with and without RVGs(loading term dominant).

Results

Validation of elementary sources against analytical solutions^[3]



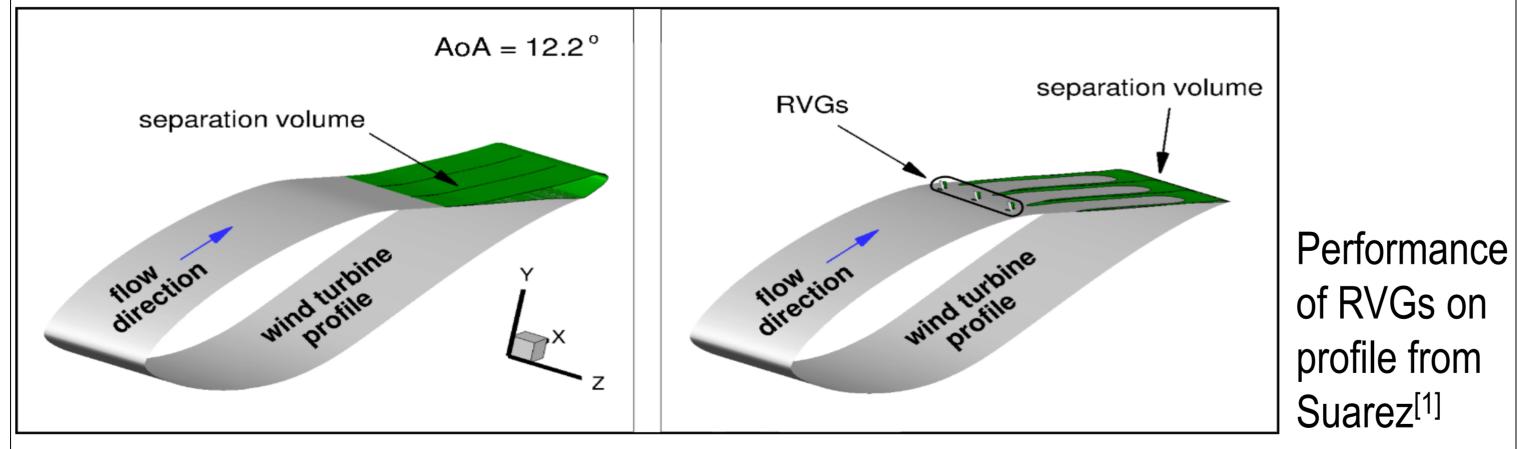


• What is their acoustic impact? Increase or decrease noise levels? **Main Objectives**

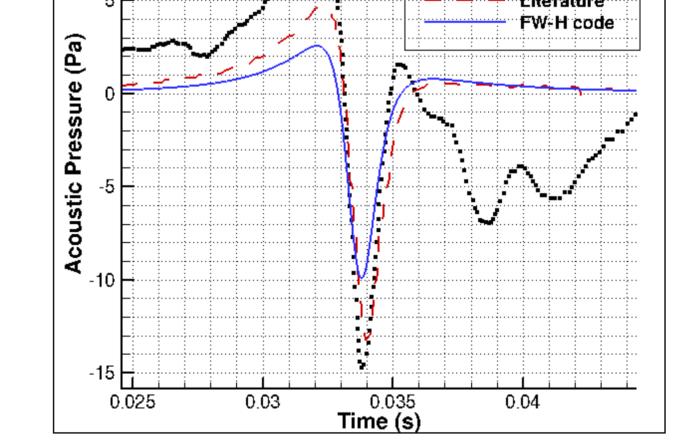
- To identify **noise sources** in the flow field for **wind turbine** blades in the **boundary layer separation** cases.
- To investigate the effect of **RVGs on noise** generated by rotor blade.

Existing Background

• Numerical investigations of **RVGs** installed on helicopter rotor and NREL wind turbine rotor show improved aerodynamic performance.

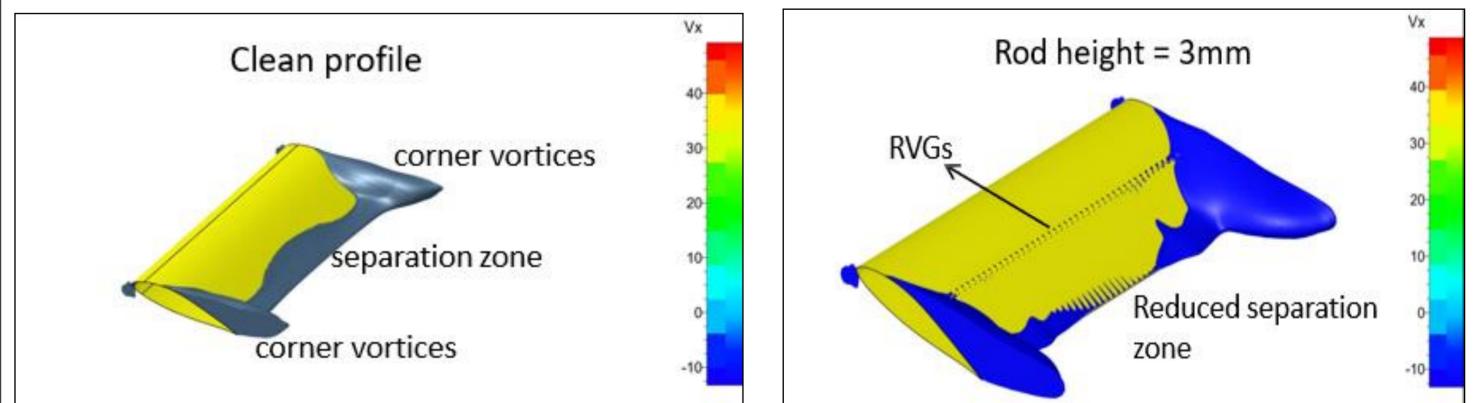


Methodology



Under-prediction of peak amplitude under analysis.

• **Design** of **RVGs** for **DU96-W-180** profile for an anechoic vertical open-jet wind tunnel at TU Delft^[5]



DU96-W-180 profile, full 3D simulation at flow velocity = 30 m/s, AoA = 13°

Future Work

- Ffowcs Williams- Hawkings (FW-H) acoustic analogy describes acoustic pressure as a sum of elementary acoustic sources such as the monopole, dipole and quadrupole.
- Aero-acoustic code development in Tecplot using macro scripting based on linear integral Farassat Formulations of FW-H in time domain. • Acoustic investigations of **rotating bodies** such as **helicopter** rotor, **wind** turbine.
- Experimental acoustic and flow (PIV) measurements for wind turbine profile **DU96-W-180 reference** case and **RVGs** case (designed to control separation) in test section at **TU Delft**.
- Steady and unsteady pressure data of NREL Phase VI rotor is under acoustic analysis using the developed aero-acoustic code.
- Secondment at TU Delft : experimental acoustic and flow measurements for **DU96-W-180** with/without RVGs.

References

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- [3] Rienstra, S. W. et al, *IWDE92-06*, 2001.
- [4] Sargent, D. C. et al, Jou. of Aircraft, 2014.
- [5] Carpio, A. R. et al, Jou. of Sound and Vibration, 2018.



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